

Linear Circuit Analysis:

Ch 11, AC Steady State Power

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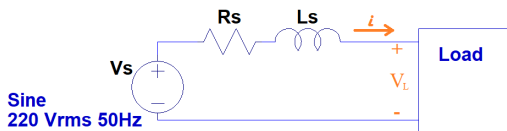
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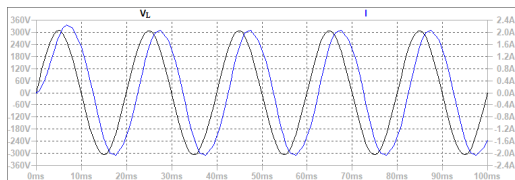
Key Concepts:

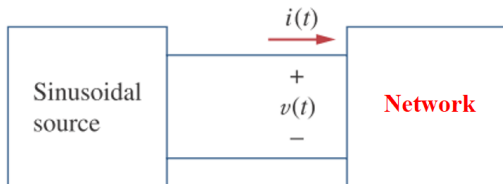
- Instantaneous power
- Average power
- Effective or rms values
- Complex power
- Power factor
- Power factor correction

Recall an AC Steady-State System



- $V_L = i \cdot Z_{\text{Load}}$





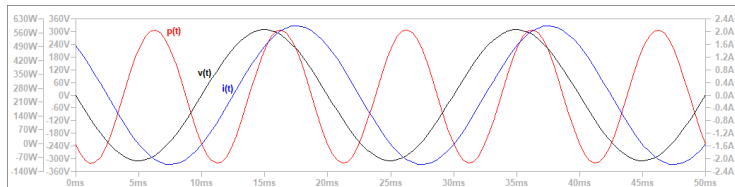
Instantaneous power:

- Instantaneous power is a power at a particular point in time.
- $p(t) = v(t) \cdot i(t)$
where $v(t)$ and $i(t)$ are voltage and current at the particular time.
- When $p(t) > 0$, the network is consuming power.
- When $p(t) < 0$, the network is supplying power.

Instantaneous Power of an AC System (I)



$$p(t) = v(t) \cdot i(t)$$



Given $v(t) = V_m \cos(\omega t + \theta_V)$ and $i(t) = I_m \cos(\omega t + \theta_I)$,

$$\begin{aligned} p(t) &= V_m \cos(\omega t + \theta_V) \cdot I_m \cos(\omega t + \theta_I) \\ &= V_m I_m \cos(\omega t + \theta_V) \cdot \cos(\omega t + \theta_I). \end{aligned}$$

Instantaneous Power of an AC System (II)



$$p(t) = V_m I_m \cos(\omega t + \theta_V) \cdot \cos(\omega t + \theta_I).$$

From a product of cosine identity:

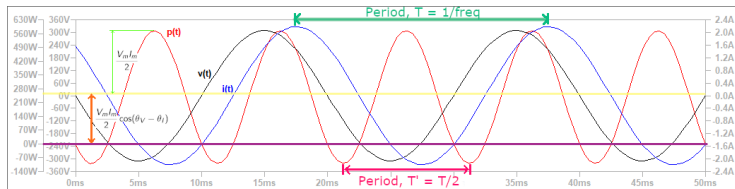
$\cos(A) \cos(B) = \frac{1}{2} \{ \cos(A - B) + \cos(A + B) \}$, therefore

$$\begin{aligned} p(t) &= \frac{V_m I_m}{2} \{ \cos(\theta_V - \theta_I) + \cos(2\omega t + \theta_V + \theta_I) \} \\ &= \underbrace{\frac{V_m I_m}{2} \cos(\theta_V - \theta_I)}_{\text{time-constant part}} + \underbrace{\frac{V_m I_m}{2} \cos(2\omega t + \theta_V + \theta_I)}_{\text{time-varying part}}. \end{aligned} \quad (1)$$



Instantaneous Power of an AC System (III)

$$p(t) = \underbrace{\frac{V_m I_m}{2} \cos(\theta_V - \theta_I)}_{\text{offset}} + \underbrace{\frac{V_m I_m}{2} \cos(2\omega t + \theta_V + \theta_I)}_{\text{sinusoid}}$$



- $\frac{V_m I_m}{2} \cos(\theta_V - \theta_I)$ (constant to time) plays an offset role.
- $\frac{V_m I_m}{2} \cos(2\omega t + \theta_V + \theta_I)$ is a sinusoidal part with its frequency doubled from the original.
 \Rightarrow its magnitude is $\frac{V_m I_m}{2}$.

Recall Properties of R, L, and C



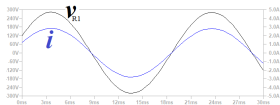
- R: $\mathbb{I} = \mathbb{V}/R = \frac{V_m}{R} \angle \theta_V$
 $\Rightarrow I$ and V are in phase: $\theta_V = \theta_I$.
- L: $\mathbb{I} = \mathbb{V}/(j\omega L) = \frac{V_m}{\omega L} \angle (\theta_V - \frac{\pi}{2})$
 $\Rightarrow I$ lags V by $\frac{\pi}{2}$: $\theta_V - \theta_I = \frac{\pi}{2}$.
- C: $\mathbb{I} = \mathbb{V} \cdot (j\omega C) = V_m \omega C \angle (\theta_V + \frac{\pi}{2})$
 $\Rightarrow I$ leads V by $\frac{\pi}{2}$: $\theta_V - \theta_I = -\frac{\pi}{2}$.

Instantaneous Power on R, L, and C (I)



$$p(t) = \underbrace{\frac{V_m I_m}{2} \cos(\theta_V - \theta_I)}_{\text{offset}} + \underbrace{\frac{V_m I_m}{2} \cos(2\omega t + \theta_V + \theta_I)}_{\text{sinusoid}}.$$

R: In phase

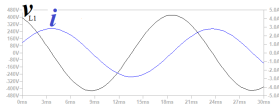


$$\theta_V = \theta_I$$

$$\Rightarrow \text{offset} = \frac{V_m I_m}{2}.$$

With this offset,
 $p_R \geq 0$ all the times.

L: Lagging by $\frac{\pi}{2}$

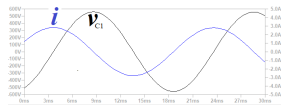


$$\theta_V - \theta_I = \frac{\pi}{2}$$

$$\Rightarrow \text{offset} = 0.$$

With no offset,
sinusoid will oscillate around 0.

C: Leading by $\frac{\pi}{2}$



$$\theta_V - \theta_I = -\frac{\pi}{2}$$

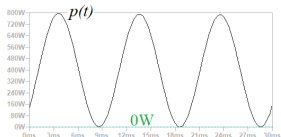
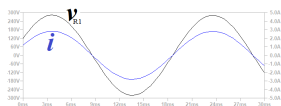
$$\Rightarrow \text{offset} = 0.$$

Instantaneous Power on R, L, and C (II)

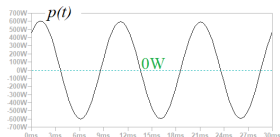
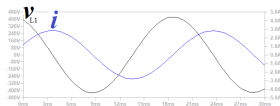


$$p(t) = \frac{V_m I_m}{2} \cos(\theta_V - \theta_I) + \frac{V_m I_m}{2} \cos(2\omega t + \theta_V + \theta_I).$$

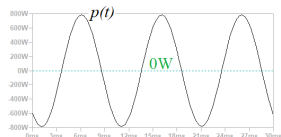
R: In phase



L: Lagging



C: Leading



$$\text{offset} = \frac{V_m I_m}{2}.$$

$p(t) \geq 0$ always.

offset = 0.

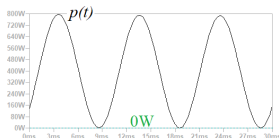
$p(t) \geq 0$ half the times

$p(t) \leq 0$ another half

Instantaneous Power on R, L, and C (III)



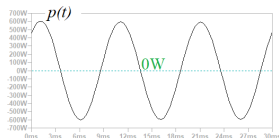
R: In phase



$p(t) \geq 0$ always.

R always consumes power.

L: Lagging



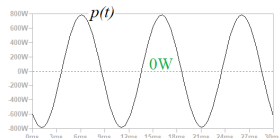
$p(t) \geq 0$ half the times
 $p(t) \leq 0$ another half

L and C are energy-storage devices.

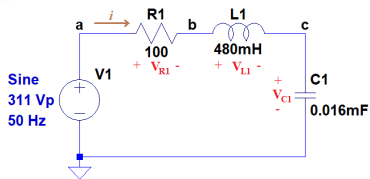
$p(t) > 0 \Rightarrow$ stores power

$p(t) < 0 \Rightarrow$ releases power

C: Leading

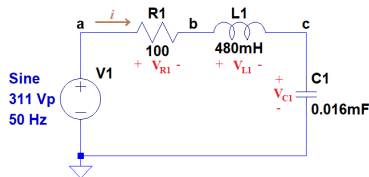


Example: Instantaneous Power (I)



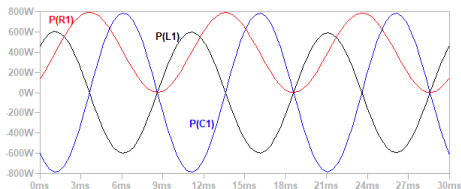
- $V_1(t) = 311 \sin(314.2t)$
- $V_1 \equiv 311 \angle -\frac{\pi}{2}$
- $Z_{R1} = 100 \Omega$
- $Z_{L1} = j150.8 \Omega$
- $Z_{C1} = -j198.9 \Omega$
- $Z = 100 - j48.1 \Omega$
- $\therefore I = V_1 / Z = 2.8 \angle -1.12$
- $i(t) = 2.8 \cos(314.2t - 1.12)$
- $V_{R1} = I \cdot Z_{R1} = 280.3 \angle -1.12$
- $V_{L1} = I \cdot Z_{L1} = 422.6 \angle 0.45$
- $V_{C1} = I \cdot Z_{C1} = 557.4 \angle -2.69$
- $V_{R1}(t) = 280.3 \cos(314.2t - 1.12)$
- $V_{L1}(t) = 422.6 \cos(314.2t + 0.45)$
- $V_{C1}(t) = 557.4 \cos(314.2t - 2.69)$

Example: Instantaneous Power (II)



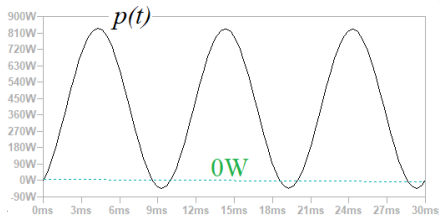
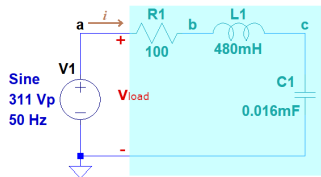
- $I_m = 2.8$; $\theta_I = -1.12$
- $V_m(R1) = 280.3$; $\theta_V(R1) = -1.12$
- $V_m(L1) = 422.6$; $\theta_V(L1) = 0.45$
- $V_m(C1) = 557.4$; $\theta_V(C1) = -2.69$
- $p_{R1}(t) = \frac{(280.3)(2.8)}{2} + \frac{(280.3)(2.8)}{2} \cos(2(314.2)t - 1.12 - 1.12)$
- $p_{L1}(t) = \frac{(422.6)(2.8)}{2} \cos(2(314.2)t + 0.45 - 1.12)$
- $p_{C1}(t) = \frac{(557.4)(2.8)}{2} \cos(2(314.2)t - 2.69 - 1.12)$

Example: Instantaneous Power (III)



- $p_{R1}(t) = 392.4 + 392.4 \cos(628.4t - 2.24)$
- $p_{L1}(t) = 591.6 \cos(628.4t - 0.67)$
- $p_{C1}(t) = 780.4 \cos(628.4t - 3.81)$

Example: Instantaneous Power (IV)



- $V_{\text{load}} = V_1$

$$\Rightarrow \therefore \underline{V}_{\text{load}} = 311 \angle -\frac{\pi}{2}$$

- $V_m(\text{load}) = 311; \theta_V(\text{load}) = -\frac{\pi}{2}$

$$\begin{aligned} p_{\text{load}}(t) &= \frac{(311)(2.8)}{2} \cos\left(-\frac{\pi}{2} + 1.12\right) + \frac{(311)(2.8)}{2} \cos\left(628.4t - \frac{\pi}{2} - 1.12\right) \\ &= 391.9 + 435.4 \cos(628.4t - 2.69) \end{aligned}$$

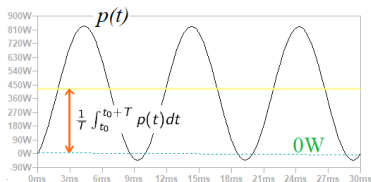


- Instantaneous power is too detailed and it tells too little about overall power consumption.

- Average Power:

$$P = \frac{1}{T} \int_{t_0}^{t_0+T} p(t) dt$$

where T is a time period; t_0 is an arbitrary point in time.



Average Power (II)



- From $p(t) = \frac{V_m I_m}{2} \cos(\theta_V - \theta_I) + \frac{V_m I_m}{2} \cos(2\omega t + \theta_V + \theta_I)$
- Thus, average power
$$P = \frac{1}{T} \int_{t_0}^{t_0+T} \left\{ \frac{V_m I_m}{2} \cos(\theta_V - \theta_I) + \frac{V_m I_m}{2} \cos(2\omega t + \theta_V + \theta_I) \right\} dt.$$
- Since integration over a period of a periodic function is 0.
$$\int_{t_0}^{t_0+T} f(t) dt = 0 \text{ when } T \text{ is a period of } f(t),$$
- then
$$P = \frac{V_m I_m}{2} \cos(\theta_V - \theta_I) + 0.$$

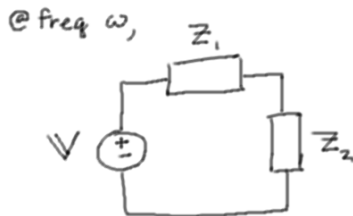
That is,

$$P = \frac{V_m I_m}{2} \cos(\theta_V - \theta_I). \quad (2)$$



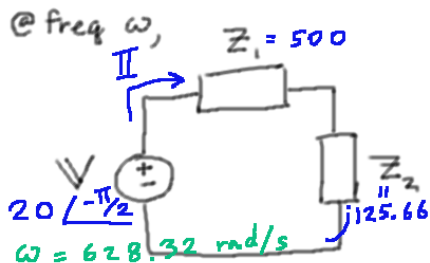
- Average power over R: $P_R = \frac{V_m I_m}{2}$
- Average power over (ideal) L: $P_L = 0$
- Average power over (ideal) C: $P_C = 0$
- Average power over an impedance $\mathbb{Z} = Z_m \angle \theta_z$: $P_Z = \frac{V_m I_m}{2} \cos \theta_z$
Recall: $\mathbb{Z} = \mathbb{V} / \mathbb{I}$ and $\theta_Z = \theta_V - \theta_I$.

Example: Average Power (I)



- Find an average power over a combination of loads Z_1 and Z_2 .
- (1) Let voltage source: $20 V_p \text{ sine } 100 \text{ Hz}$;
 Z_1 is a 500Ω resistor and Z_2 is a 200mH inductor.
- (2) Let voltage source: $10 V_{pp} \text{ cosine } 10 \text{ Hz}$; Z_1 is a $1\text{k}\Omega$ resistor and Z_2 is a $16\mu\text{F}$ inductor.

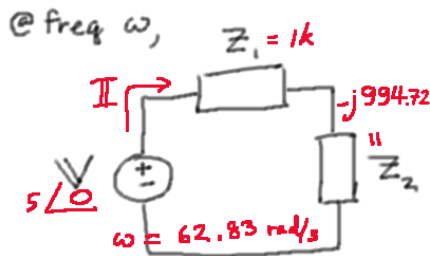
Example: Average Power (II)



$$I = V / (Z_1 + Z_2) = 0.0388 \angle -1.817.$$

$$P = \frac{(20)(0.0388)}{2} \cos\left(-\frac{\pi}{2} + 1.817\right)$$

$$\therefore P = 0.3763 \text{ W.}$$



$$I = 3.54 \text{ m} \angle 0.783.$$

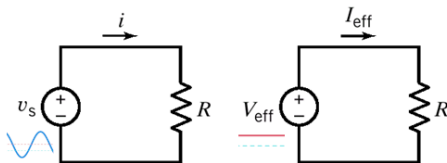
$$P = \frac{(5)(3.54 \text{ m})}{2} \cos(0 - 0.783)$$

$$\therefore P = 6.59 \text{ mW.}$$

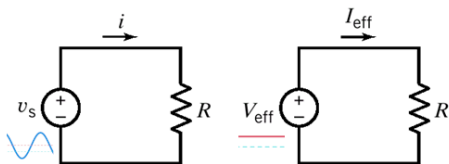


- An AC voltage can be described in many ways: peak value V_p , peak-to-peak value V_{pp} , magnitude $V_m = V_p$, or amplitude $V_a = V_m = V_p$.
- How are these quantities compared to a DC voltage?
⇒ Rationale is to describe a magnitude of an AC voltage in a way to comprehend its real work.
- I.e., describing the magnitude of an AC voltage by an amount of a DC voltage that will deliver the same average power to a resistor.

Effective Values (II)



- V_{eff} : an amount of a dc voltage that delivers the same average power as its counterpart V_s .
- Average power on R by an AC voltage
$$P_{ac} = \frac{1}{T} \int_0^T \frac{v_s^2}{R} dt$$
- Average power on R by a DC voltage
$$P_{eff} = \frac{v_{eff}^2}{R}.$$



Solve for v_{eff} (delivering the same power as v_s):

$$v_{eff} = \sqrt{\frac{1}{T} \int_0^T v_s^2 dt}. \quad (3)$$

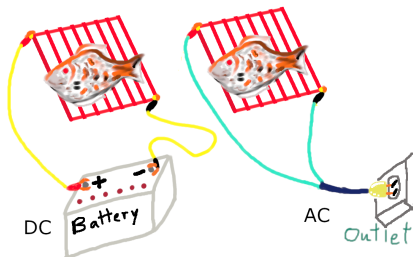
- Since the result is obtained by squaring, averaging, and finding a square root, it is called a “Root-Mean-Square” value or “RMS” for short.

Effective Values (IV)



- The effective value of an ac voltage is the amount of its dc equivalence, i.e., supplying the same average power on a resistor.
- So is an effective value of an ac current.

$$v_{rms} = \sqrt{\frac{1}{T} \int_0^T v_s^2 dt} \quad i_{rms} = \sqrt{\frac{1}{T} \int_0^T i_s^2 dt}$$



Effective voltage is like finding a dc equivalence to cook the fish as if the fish is cooked by an ac.

RMS on Sinusoid



Given $v_s(t) = V_m \cos(\omega t)$,

$$\begin{aligned} V_{rms} &= \sqrt{\frac{1}{T} \int_0^T (V_m \cos(\omega t))^2 dt} \\ &= V_m \sqrt{\frac{1}{T} \int_0^T \cos^2(\omega t) dt} \\ &= V_m \sqrt{\frac{1}{T} \int_0^T \frac{1 + \cos(2\omega t)}{2} dt} \\ &= V_m \sqrt{\frac{1}{2} \cdot \underbrace{\frac{1}{T} \int_0^T 1 dt}_1 + \underbrace{\frac{1}{T} \int_0^T \frac{\cos(2\omega t)}{2} dt}_0} \\ &= \frac{V_m}{\sqrt{2}}. \end{aligned} \tag{4}$$

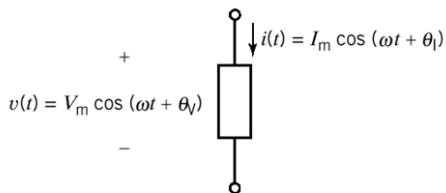


- $V_{rms} = \frac{V_m}{\sqrt{2}}$
- $I_{rms} = \frac{I_m}{\sqrt{2}}$

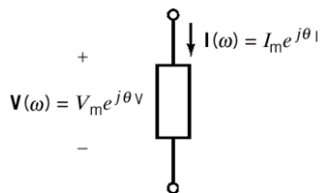
⇒ Conveniently, average power

$$\begin{aligned} P &= \frac{V_m \cdot I_m}{2} \cos(\theta_V - \theta_I) \\ &= \frac{V_m}{\sqrt{2}} \cdot \frac{I_m}{\sqrt{2}} \cos(\theta_V - \theta_I) \\ &= V_{rms} \cdot I_{rms} \cos(\theta_V - \theta_I). \end{aligned}$$

Complex Power (I)



Time domain



Frequency domain

- voltage and current can be represented in frequency domain as complex numbers.
- So is power!

Complex Power (I)



Given $\mathbb{V} = V_m \angle \theta_V$ and $\mathbb{I} = I_m \angle \theta_I$, complex power delivered to the element is defined as:

$$\begin{aligned} \mathbb{S} &= \frac{\mathbb{V} \cdot \mathbb{I}^*}{2} = \frac{(V_m \angle \theta_V) \cdot (I_m \angle -\theta_I)}{2} \\ &= \frac{V_m \cdot I_m}{2} \angle (\theta_V - \theta_I) \\ &= V_{rms} \cdot I_{rms} \angle (\theta_V - \theta_I) \end{aligned} \quad (5)$$

where \mathbb{I}^* is a complex conjugate of \mathbb{I} .



Complex Power (II)

- Complex power $S = \frac{V_m \cdot I_m}{2} \angle(\theta_V - \theta_I)$.
- Magnitude $|S| = \frac{V_m \cdot I_m}{2}$ is called “apparent power”.
- Its rectangular form:

$$S = \underbrace{\frac{V_m \cdot I_m}{2} \cos(\theta_V - \theta_I)}_P + j \underbrace{\frac{V_m \cdot I_m}{2} \sin(\theta_V - \theta_I)}_Q$$

$$S = P + jQ.$$

- Its real part P is average power or real power.
- Its imaginary part Q is called “reactive power”.
- S 's unit is VA (Volt-Amp).

P 's is W.

Q 's is VAR (Volt-Amp Reactive).



- Complex power $\mathbb{S} = \underbrace{\frac{V_m \cdot I_m}{2} \cos(\theta_V - \theta_I)}_P + j \underbrace{\frac{V_m \cdot I_m}{2} \sin(\theta_V - \theta_I)}_Q$.
- Real power $P = \underbrace{\frac{V_m \cdot I_m}{2}}_{|\mathbb{S}|} \cdot \underbrace{\cos(\theta_V - \theta_I)}_{\text{power factor}}$.
- Power factor $pf = \cos(\theta_V - \theta_I)$.
- pf angle $\theta_V - \theta_I > 0 \Rightarrow$ “lagging”
Current lags voltage \rightarrow inductive load.
- pf angle $\theta_V - \theta_I = 0 \Rightarrow$ “in-phase”
Current and voltage are in-phase \rightarrow purely resistive load.
- pf angle $\theta_V - \theta_I < 0 \Rightarrow$ “leading”
Current leads voltage \rightarrow capacitive load.

Example: Load Impedance (I)



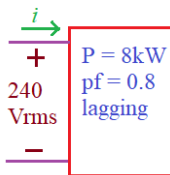
An electric load operates at 240 Vrms. The load consumes an average power of 8 kW at a lagging power factor of 0.8.

- Calculate the complex power of the load.
- Calculate the impedance of the load.

Solution for (a):

- $pf = \cos(\phi) = 0.8$ and $P = 8kW = |\mathbb{S}| \cdot \cos(\phi)$.
 $\Rightarrow |\mathbb{S}| = 8k/0.8 = 10 \text{ kVA}$.
- lagging $\Rightarrow \phi > 0$.
 $\Rightarrow \phi = \cos^{-1} 0.8 = 0.6435 \text{ rad}$.
- $\therefore Q = |\mathbb{S}| \cdot \sin(\phi) = 10k \sin(0.6435) = 6 \text{ kVAR}$.
- $\mathbb{S} = P + jQ = 8 + j6 \text{ kVA}$.

Example: Load Impedance (II)

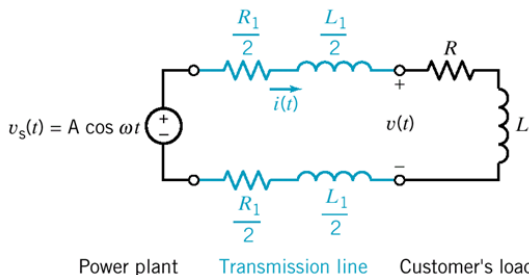


Solution for (b):

- $P = 8kW = \frac{V_m I_m}{2} \cdot pf = V_{rms} \cdot I_{rms} \cdot pf = 240 \cdot I_{rms} \cdot 0.8$
 $\Rightarrow I_{rms} = 41.67 \text{ A.}$
- Impedance $Z = \frac{V}{I} = \frac{V_m}{I_m} \angle(\theta_V - \theta_I) = \frac{V_{rms}}{I_{rms}} \angle\phi = \frac{240}{41.67} \angle 0.6435$.
 $\Rightarrow Z = 4.608 + j3.456 \Omega.$



The transmission lines for electrical power



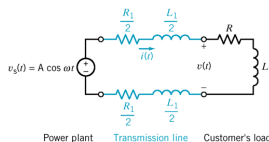
- Transmission lines are significantly different from ideal wires.

$$\mathbb{Z}_{line} = R_1 + j\omega L_1.$$

- Average power losing on the lines

$$P_{line} = I_{rms}^2 \cdot \text{Re}\{\mathbb{Z}_{line}\} = I_{rms}^2 R_1.$$

PF and Transmission Loss (II)

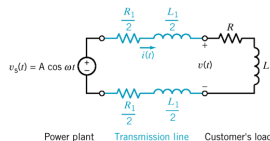


Average power losing on the lines

$$P_{line} = I_{rms}^2 \cdot \text{Re}\{Z_{line}\} = I_{rms}^2 R_1.$$

- A large load is often inductive, e.g., machine, motor, pump, etc.
- Power consumed by the load is what its owner pays.
$$P_{load} = V_{rms} I_{rms} \cdot pf.$$
- Power losing on the lines is just a waste of energy, which customers do not pay, but it costs an electric supplier.
- Given the same P_{load} and operating voltage V_{rms} , a lower pf causes a higher current I_{rms} . And, a higher current $I_{rms} \Rightarrow$ a higher P_{line} .

PF and Transmission Loss (III)



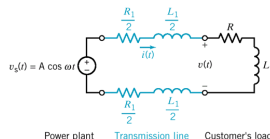
$$P_{load} = V_{rms} I_{rms} \cdot pf.$$

$$P_{line} = I_{rms}^2 \cdot \text{Re}\{Z_{line}\} = I_{rms}^2 R_1.$$

Example: a 1.4kW Load with a lagging power factor of 0.8, operated at 220 V_{rms} 50Hz.

- Current i drawn by the load: $I_{rms} = \frac{1.4k}{(220)(0.8)} = 7.95 \text{ A}.$
- Supposed $R_1 = 1 \Omega$, $P_{line} = (7.95)^2(1) = 63.27 \text{ W}.$
 \Rightarrow To put it in perspective, if the load is run 20 hr/day, 350 days a year, that counts 7000 hours. Supposed the price is 5 baht/unit, energy loss:
 $E_{loss} = (63.27)(7000) = 442890 \text{ Wh} = 442.89 \text{ units}.$
Thus, estimated loss is 2214.45 baht for this one customer.

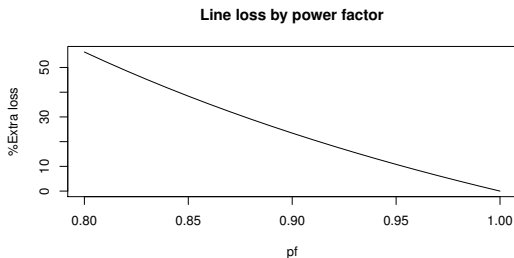
PF and Transmission Loss (III)



$$I_{rms} = \frac{P_{load}}{V_{rms} \cdot pf}$$
$$P_{line} = I_{rms}^2 R_1$$

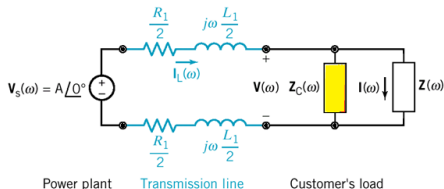
Line loss as a function of power factor

$$P_{line} = \left(\frac{P_{load}}{V_{rms} \cdot pf} \right)^2 R_1$$



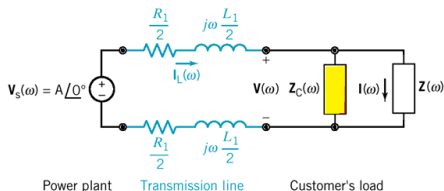
With pf of 0.8, the power line loss is over 50% of the ideal case ($pf = 1$).

Power Factor Correction (I)



- To mitigate, a customer is required to have the power factor above an agreeable level.
- To “correct” power factor of a load, a correcting impedance is installed across the terminals of the customer’s load.
⇒ having the correcting impedance parallel to the load retains the load operating voltage.

Power Factor Correction (II)



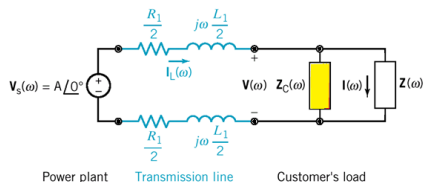
The correcting impedance should turn power factor of the load to

$$pfc = \cos \phi_p,$$

where pfc and ϕ_p are the target power factor and the target pf angle.

Given load impedance $\mathbb{Z} = R + jX$ and correcting impedance $\mathbb{Z}_c = R_c + jX_c$, the correcting impedance should not consume power itself: $R_c = 0 \Rightarrow \mathbb{Z}_c = jX_c$. (It must be purely reactive, C or L.)

Power Factor Correction (III)



Target power factor: $pf_c = \cos \phi_p$.

Original load: $Z = R + jX$.

Correcting impedance: $Z_c = jX_c$.

- corrected impedance: $Z_p = \frac{ZZ_c}{Z+Z_c} = R_p + jX_p = Z_p \angle \theta_p$.
- note: pf angle = load angle, i.e., $\theta_p = \phi_p$.
 $\Rightarrow Z_p = Z_p \angle \phi_p$
 $\Rightarrow \phi_p = \tan^{-1} \frac{X_p}{R_p} \Rightarrow pf_c = \cos(\tan^{-1} \frac{X_p}{R_p}) \Rightarrow \frac{X_p}{R_p} = \tan(\cos^{-1} pf_c)$.

Power Factor Correction (IV)



$$(1) \mathbb{Z}_p = \frac{\mathbb{Z}\mathbb{Z}_c}{\mathbb{Z} + \mathbb{Z}_c} = R_p + jX_p.$$

Target: $pf = \cos \phi_p$.

$$(2) \frac{X_p}{R_p} = \tan(\cos^{-1} pf).$$

Impedances: $\mathbb{Z} = R + jX$ and $\mathbb{Z}_c = jX_c$.

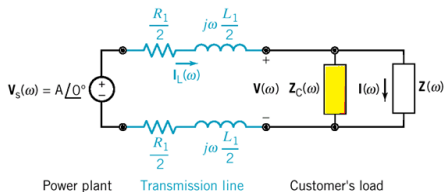
Work the math, from (1):

$$\mathbb{Z}_p = \frac{(R + jX)(jX_c)}{(R + jX) + jX_c} = \underbrace{\frac{RX_c^2}{R^2 + (X + X_c)^2}}_{R_p} + j \underbrace{\frac{R^2X_c + (X_c + X)XX_c}{R^2 + (X + X_c)^2}}_{X_p}.$$

Put the result into (2):

$$\frac{R^2X_c + (X_c + X)XX_c}{RX_c^2} = \tan(\cos^{-1} pf).$$

Power Factor Correction (V)

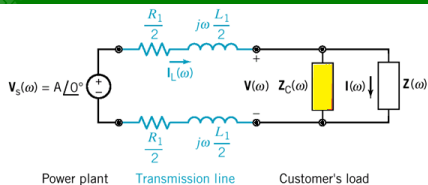


Solve for X_c in terms of R , X , and pf_c :

$$X_c = \frac{R^2 + X^2}{R \tan(\cos^{-1} pf_c) - X}. \quad (6)$$



Example: Power Factor Correction



Reactive value:

$$X_C = \frac{R^2 + X^2}{R \tan(\cos^{-1} pfc) - X}$$

Example. A 1.4kW load with a lagging pf of 0.8, operating at 220 Vrms 50 Hz, is required to be corrected for pf of 0.95.

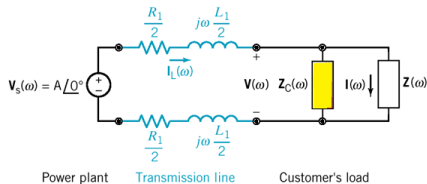
Solution:

Recalling from the previous example, $I_{rms} = 7.95$ A. Then,

$$Z = \frac{220}{7.95} \angle \left(\underbrace{+}_{\text{lagging}} \cos^{-1} 0.8 \right) = 27.67 \angle 0.64 = 22.19 + j16.52 \Omega.$$

Thus, $X_C = \frac{22.19^2 + 16.52^2}{22.19 \cdot \tan(\cos^{-1} 0.95) - 16.52} = -82.9$. Since $X_C < 0$, the correcting impedance must be capacitive: $X_C = -\frac{1}{\omega C}$. Given $\omega = 2\pi(50) = 314.16$ rad/s, $C = 38.4 \mu\text{F}$ (or larger).

Power Factor Correction: Inductive Load (I)



Reactive value:

$$X_c = \frac{R^2 + X^2}{R \tan(\cos^{-1} pfc) - X}$$

- The larger pfc (closer to 1), the better.
- $pfc \rightarrow 1 \Rightarrow \cos^{-1} pfc \rightarrow 0 \Rightarrow \tan(\cos^{-1} pfc) \rightarrow 0$.
- Sign of X_c is opposite to the sign of X .
 - \Rightarrow Correct capacitive load with inductor.
 - \Rightarrow Correct inductive load with capacitor.

Power Factor Correction: Inductive Load (II)



Typical loads are inductive. Thus, $X_c = -\frac{1}{\omega C}$ and

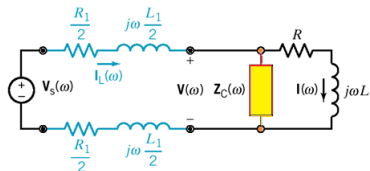
$$\begin{aligned}-\frac{1}{\omega C} &= \frac{R^2 + X^2}{R \tan(\cos^{-1} pfc) - X} \\ \omega C &= \frac{X - R \tan(\cos^{-1} pfc)}{R^2 + X^2} \\ &= \frac{R}{R^2 + X^2} \cdot \left(\frac{X}{R} - \tan(\cos^{-1} pfc) \right).\end{aligned}$$

Given an original pf angle $\phi = \tan^{-1} \frac{X}{R}$, hence

$$C = \frac{R}{\omega \cdot (R^2 + X^2)} \cdot (\tan \phi - \tan \phi_c), \quad (7)$$

where $\phi = \cos^{-1} pf$ and $\phi_c = \cos^{-1} pfc$.

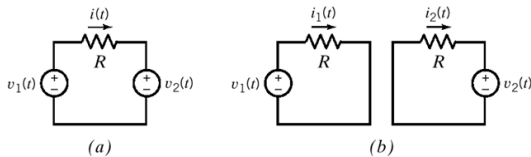
Example: Power Factor Correction on Inductive Load



Given the original load $Z = 100 + j100 \Omega$ at 60 Hz, find C to improve pf to 0.95.

Solution:

- $\phi = \tan^{-1} \frac{X}{R} = 0.785 \text{ rad.}$
- $\phi_c = \cos^{-1} pfc = 0.318 \text{ rad.}$
- $\omega = 2\pi f = 377 \text{ rad/s.}$
- $C = \frac{100}{377 \cdot (100^2 + 100^2)} \cdot (\tan 0.785 - \tan 0.318) = 8.9 \mu\text{F (or larger).}$

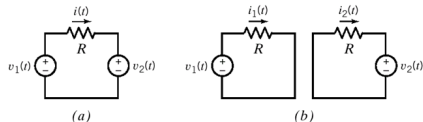


- Superposition: $i = i_1 + i_2$.
- Instantaneous power: $p = i^2 R = (i_1 + i_2)^2 R = (i_1^2 + i_2^2 + 2i_1 i_2) R$.

Average power:

$$\begin{aligned}
 P &= \frac{1}{T} \int_0^T p(t) dt = \frac{1}{T} \int_0^T (i_1^2 + i_2^2 + 2i_1 i_2) R dt \\
 &= P_1 + P_2 + \frac{2R}{T} \int_0^T (i_1 \cdot i_2) dt.
 \end{aligned}$$

Power Superposition for Multi-Frequency Excitation (II)



Average power:

$$P = P_1 + P_2 + \underbrace{\frac{2R}{T} \int_0^T (i_1 \cdot i_2) dt}$$

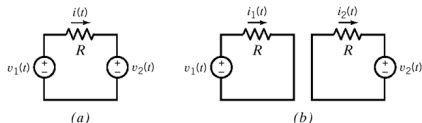
Given $i_1 = I_1 \cos(\omega_1 t + \theta_1)$ and $i_2 = I_2 \cos(\omega_2 t + \theta_2)$,

$$\int_0^T (i_1 \cdot i_2) dt = I_1 I_2 \int_0^T \cos(\omega_1 t + \theta_1) \cos(\omega_2 t + \theta_2) dt.$$

$$\text{From } \cos A \cos B = \frac{\cos(A-B) + \cos(A+B)}{2},$$

$$\begin{aligned} \int_0^T (i_1 \cdot i_2) dt &= \frac{I_1 I_2}{2} \int_0^T (\cos((\omega_1 - \omega_2)t + \theta_1 - \theta_2)) dt \\ &+ \underbrace{\frac{I_1 I_2}{2} \int_0^T (+ \cos((\omega_1 + \omega_2)t + \theta_1 + \theta_2)) dt}_0 \end{aligned}$$

Power Superposition for Multi-Frequency Excitation (II)



Average power:

$$P = P_1 + P_2 + \underbrace{\frac{2R}{T} \int_0^T (i_1 \cdot i_2) dt}$$

$$\begin{aligned} \int_0^T (i_1 \cdot i_2) dt &= \frac{I_1 I_2}{2} \int_0^T (\cos((\omega_1 - \omega_2)t + \theta_1 - \theta_2)) dt \\ &= \begin{cases} 0 & \text{for } \omega_1 \neq \omega_2, \\ \frac{I_1 I_2 T}{2} \cos(\theta_1 - \theta_2) & \text{for } \omega_1 = \omega_2. \end{cases} \end{aligned}$$

That is,

$$P = P_1 + P_2 + \begin{cases} 0 & \text{for } \omega_1 \neq \omega_2, \\ I_1 I_2 R \cos(\theta_1 - \theta_2) & \text{for } \omega_1 = \omega_2. \end{cases} \quad (8)$$



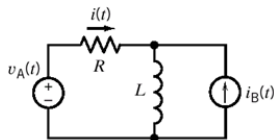
“The average power delivered to a circuit by several sinusoidal sources, acting together, is equal to the sum of the average power delivered to the circuit by each source acting alone, **if and only if no two of the sources have the same frequency.**”

$$\begin{aligned} P_{total} &= P_1 + P_2 + \cdots + P_N \\ &= \sum_i P_i, \end{aligned}$$

where P_i is a power computed as if the i^{th} sinusoidal source acting alone and no two sources have the same frequency.

Caution! Superposition principle cannot be applied to power in general.

Example: Power Superposition (I)



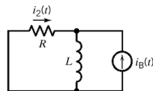
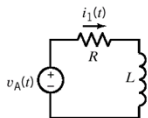
Find power P_R consumed by R in this setting: $v_A(t) = 155.6 \cos(377t)$;
 $i_B(t) = 1.2 \cos(314.16t)$;
 $R = 50 \Omega$ and $L = 0.5 \text{ H}$.

Solution:

- Both sources have different frequencies.
 \Rightarrow use superposition to work on one source at a time.
- Since both sources are sinusoidal and have different frequencies, power superposition can be applied.

$$P_R = P_R(v_A) + P_R(i_B).$$

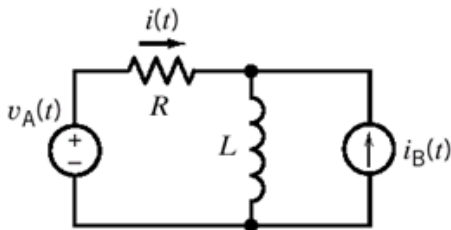
Example: Power Superposition (II)



- $\omega_1 = 377 \text{ rad/s}$
- $Z_R = 50; Z_L = j188.5.$
- $V_A = 155.6 \angle 0.$
- $I_1 = \frac{V_A}{50 + j188.5}$
 $= 0.798 \angle -1.31$
- $P_R(v_A) = I_{1rms}^2 R$
 $= \left(\frac{0.798}{\sqrt{2}}\right)^2 50 = 15.92 \text{ W}.$

- $\omega_2 = 314.16 \text{ rad/s}$
- $Z_R = 50; Z_L = j157.08.$
- $I_B = 1.2 \angle 0.$
- $I_2 = -I_B \cdot \frac{Y_R}{Y_R + Y_L}$
 $= -1.2 \frac{(1/50)}{(1/50) + (1/j157.08)}$
 $= 1.143 \angle -2.83.$
- $P_R(i_B) = I_{2rms}^2 R$
 $= \left(\frac{1.143}{\sqrt{2}}\right)^2 50 = 32.69 \text{ W}.$

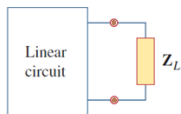
Example: Power Superposition (III)



Since both sources have different frequency, the power superposition is valid:

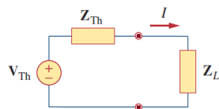
$$\begin{aligned} P_R &= P_R(v_A) + P_R(i_B) \\ &= 15.92 + 32.69 = 48.61 \text{ W}. \end{aligned}$$

Maximum Average Power Transfer (I)



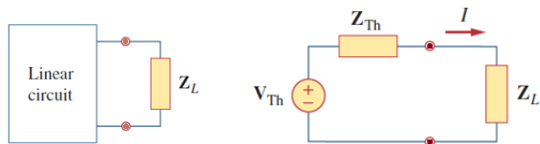
- At some situation, we may want to find a load Z_L such that the power delivered to the load is maximum.

- To simplify the task, the port circuit is modeled by Thevenin equivalent circuit.



- Supposed $Z_{Th} = R_{Th} + jX_{Th}$ and $Z_L = R_L + jX_L$, current $I = \frac{V_{Th}}{Z_{Th} + Z_L}$.
- Average power $P_R = \frac{V_m I_m}{2} = \frac{1}{2} I_m^2 R_L = \frac{1}{2} \frac{|V_{Th}|^2 R_L}{(R_{Th} + R_L)^2 + (X_{Th} + X_L)^2}$
- Find X_L and R_L maximizing P_R .

Maximum Average Power Transfer (II)



$$P_R = \frac{1}{2} \frac{|\mathbb{V}_{Th}|^2 R_L}{(R_{Th} + R_L)^2 + (X_{Th} + X_L)^2}$$

- Notice that $X_L = -X_{Th}$ maximizing P_R .
- Solve $\frac{\partial P_R}{\partial R_L} = 0$ for R_L
 $\Rightarrow R_L = R_{Th}$.

Thus,

$$\mathbb{Z}_L = R_{Th} - jX_{Th} = \mathbb{Z}_{Th}^* \quad (9)$$

The maximum power is:

$$P_{\max} = \frac{|\mathbb{V}_{Th}|^2_{Th}}{8R_{Th}} \quad (10)$$

Example: Maximum Average Power Transfer (I)



Determine the load impedance Z_L maximizing the average power drawn from the circuit.

What is the maximum average power?

Solution:

- Firstly, find Thevenin equivalent circuit.

$$\Rightarrow (\text{V divider}) \quad V_{oc} = 10 \cdot \frac{8-j6}{4+8-j6} = 7.454 \angle -0.18.$$

\Rightarrow (Mesh analysis)

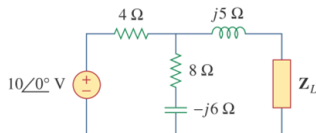
$$-10 + 4I_1 + (8 - j6)(I_1 - I_2) = 0.$$

$$(8 - j6)(I_2 - I_1) + j5I_2 = 0.$$

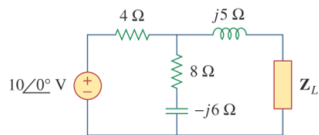
Solve for $I_2 = I_{sc} = 1.395 \angle -1.1696$.

$$\Rightarrow V_{Th} = V_{oc} = 7.454 \angle -0.18.$$

$$\Rightarrow Z_{Th} = V_{oc}/I_{sc} = 2.93 + j4.47.$$



Example: Maximum Average Power Transfer (II)



$$\mathbb{V}_{Th} = 7.454 \angle -0.18.$$

$$\mathbb{Z}_{Th} = 2.93 + j4.47.$$

- $\mathbb{Z}_L = \mathbb{Z}_{Th}^* = 2.93 - j4.47 \Omega.$
- $P_{\max} = \frac{|\mathbb{V}_{Th}|_{Th}^2}{8R_{Th}} = \frac{7.454^2}{8(2.93)} = 2.37 \text{ W}.$



David E. Johnson, Johnny R. Johnson, John L. Hilburn, and Peter D. Scott,
Electric Circuit Analysis. Wiley 3rd edition (January 15, 1997).